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1 **Interpretation of DGT measurements. Review of a systematic**
2 **approach.**

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7 **Environmental Context**

8 Dynamic speciation of a given element in a natural medium is key
9 for understanding its availability. DGT has become a widely used
10 tool for in-situ environmental studies, being applied to determine
11 fluxes of metal cations (Zn, K, Fe..), anions (such as phosphate),
12 organics, antibiotics, nanoparticles, etc.. The interpretation of the
13 measurements with suitable physicochemical models gives valuable
14 insights on the behavior of the system.
15

16 **Abstract**

17 Gaining insight into the physicochemical processes integrated in a DGT (Diffusion
18 Gradients in Thin Films) measurement and combining them in a model can assist in
19 retrieving fundamental information, both qualitative and quantitative, on the probed
20 system. New experiments (such as varying the thicknesses of the gel and/or the resin
21 layer) and their mathematical treatment to extract meaningful parameters have been
22 suggested from theoretical considerations. The concept of lability degree is useful in
23 describing an interpretation of the DGT-concentration as the summation of the free metal
24 concentration plus the labile fraction of all complexes multiplied by a ratio of diffusion
25 coefficients. In some cases, the lability degree can be directly estimated with specific
26 measurements and a very simple expression. We review the current status of these
27 interpretations, including numerical simulations, with special focus on analytical
28 expressions, because they can be more accessible to the standard DGT practitioner.
29 Present limitations and challenges for future work in DGT interpretation are also
30 discussed.

31 **1. Introduction**

32 Since its presentation in 1994,^[1] DGT (Diffusive Gradients in Thin Films) has reached an
33 extraordinary success in the scientific community working in environmental speciation
34 and availability. There are many reasons for this success, from its simple conceptual
35 design to the practical availability of accurately manufactured devices. The amplitude of
36 applications^[2] arises not only from the variety of media (waters,^[3] sediments,^[4,5] soils,^[6]
37 etc.), but also from the variety of analytes (heavy metals,^[7,8] lanthanides,^[9,10] K,^[11]
38 phosphate,^[12,13] As, V, Sb, Mo, W,^[14] Fe,^[15] nanoparticles,^[16,17] antibiotics,^[18]..) and also
39 from its designed *in situ* measurement capacity.^[19]

40 Theoretical contributions have also been developed^[20-25] to interpret the measurements
41 and even have been able to suggest new experiments to gain more information about the
42 probed system. Numerical models, analytical expressions and experimental approaches
43 complement and reinforce each other helping in unraveling the system characteristics.
44 However, any model is a simplification of the reality. So it is essential to judiciously
45 choose the most relevant phenomena and neglect the rest, keeping a balance between
46 simplicity (few selected phenomena, simpler geometries, limiting regimes, etc.) and
47 sufficient accuracy in the predicted response. For instance, the resin layer is in reality a
48 3D entity with resin beads tending to be denser close to the resin/gel interface (due to the
49 settling preparation of the resin layer), but analytical expressions could not be derived for
50 such a 3D model.

51 Here, we review a DGT interpretation which essentially relies on physicochemical
52 modeling of diffusion and complex dissociation. The primary environmental context in
53 mind corresponds to heavy metals in aqueous media, but other media (such as soil or
54 sediments) or other analytes could also be considered.

55

56 The structure of this work is as follows. In section 2, the direct information provided by
57 accumulation and fluxes is linked to the concept of lability degree. This will allow an
58 interpretation of the DGT-concentration in section 3. Section 4 considers the “Penetration
59 Analytical Model”, PAM, which is progressively extended to include mixtures (section
60 5), the diffusive boundary layer (section 6) or electrostatic effects (section 7). Limitations
61 and prospects are briefly suggested in section 8.

62

63 **2. Key concepts: accumulation, fluxes and lability degree**

64 A DGT device consists of a resin layer (with thickness r), covered with a diffusive gel
65 layer (of thickness g) and a filter in contact with the probed phase (in principle, aqueous
66 solution in this work) where a diffusive boundary layer, DBL (of thickness δ) can
67 develop. Let n_M be the number of moles of the analyte (M for simplicity) accumulated in
68 the resin at a given time (t). The flux, can be computed as:

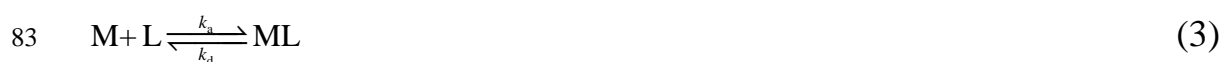
$$69 \quad J(t) = \frac{1}{A} \frac{dn_M}{dt} \quad (1)$$

70 where A is the effective area of the gel-solution interface. A detailed plot of the
71 accumulated n_M in front of increasing deployment times would reveal 4 regimes: transient
72 (when the flux is growing), (quasi) steady-state regime (practically constant flux),
73 approach to equilibrium (decreasing flux) and equilibrium (null flux)^[26,27]. The practical
74 use of DGT has consisted in focusing in the steady-state regime (while neglecting the
75 very small effects of the short transient regime), so that, the time integral of the flux
76 becomes just

$$77 \quad n_M = JAt \quad (2)$$

78 Thus, from the processing of the accumulations, DGT is also providing a quantification
79 of the flux.

80 This steady-state flux will result from the contributions by the arrival of free M and other
 81 M-containing species to the sensor. For simplicity, let us start assuming that just one
 82 complex ML is formed with a ligand L:



84 The stability constant K (ratio of the association and dissociation kinetic constants, k_a and
 85 k_d) rules the concentration in the bulk (denoted with superscript *) of the sampled
 86 solution:

$$87 \quad K = \frac{k_a}{k_d} = \frac{c_{\text{ML}}^*}{c_{\text{M}}^* c_{\text{L}}^*} \quad (4)$$

88 For vanishing values of the rate constants, the inert complex does not dissociate and the
 89 free metal J_{free} would be the only contribution to the total flux. For extremely high values
 90 of the rate constants, metal and complex are in equilibrium at all points and the resulting
 91 flux (J_{lab}) is termed fully labile. The extent of the participation of the complex to the total
 92 flux can be quantified by the lability degree ξ ^[28] of the complex:

$$93 \quad \xi \equiv \frac{J - J_{\text{free}}}{J_{\text{labile}} - J_{\text{free}}} \quad (5)$$

94 With this definition, $\xi=0$ for an inert complex and $\xi=1$ for a fully labile one.

95

96 It can be shown^[28,29], that, for systems with only one ligand and vanishing concentration
 97 of M at the resin-gel interface ($x=r$), the lability degree is directly connected to the
 98 normalized concentration of ML at that point:

$$99 \quad \xi = 1 - \frac{c_{\text{ML}}^r}{c_{\text{ML}}^*} \quad (6)$$

100 where the superscript r indicates the concentration of ML at $x=r$.

101

102 From the definition of ξ (5),

$$103 \quad J = J_{\text{free}} + \xi (J_{\text{labile}} - J_{\text{free}}) \quad (7)$$

104

105 For trace speciation measurements, usually J_{free} is negligible as the amount of free metal
 106 is very low (one could label this as “overwhelming complex” conditions). Under these
 107 conditions, and if the diffusion coefficient of the complex is known or can be estimated,
 108 one can compute the lability degree as:

$$109 \quad \xi \approx \frac{J}{J_{\text{labile}}} \approx \frac{n_{\text{M}} / (At)}{\left(\frac{D_{\text{ML}}}{D_{\text{M}}}\right) n_{\text{M}}^{\text{no-ligand}} / (At)} = \frac{D_{\text{M}} n_{\text{M}}}{D_{\text{ML}} n_{\text{M}}^{\text{no-ligand}}} \quad (8)$$

110 where the labile flux has been estimated from the accumulation of M in the same system,
 111 but without ligand (i.e. just the metal) and a re-scaling by a factor to take into account the
 112 different diffusion coefficients of the complex (D_{ML}) and of the metal (D_{M}). In this sense,
 113 the lability degree can be interpreted as a normalised flux (where diffusion coefficients
 114 and not only accumulated amounts are involved).

115

116 The definition of a global lability degree (5) can be extended to a system with any number
 117 of ligands, and can be approximated with eqn. (8) if all complexes have a similar diffusion
 118 coefficient D_{ML} .

119

120 **3. What is DGT-concentration?**

121 From the steady-state solution of Fick’s second law for just one species in planar
 122 geometry, and assuming that the concentration of this species M vanishes at the resin-gel
 123 interface, the simple expression^[1] follows

$$124 \quad n_{\text{M}} = A \left(\frac{D_{\text{M}} c_{\text{DGT}}}{g} \right) t \quad (9)$$

125 (where the thickness of the gel g could include the filter and DBL thickness in some
 126 cases^[2]). Provided that the diffusion coefficient of free metal is used for D_M in eqn. (9),
 127 this can be taken as an operational definition of the DGT-concentration, c_{DGT} . Its physical
 128 meaning is quite simple: c_{DGT} is the metal concentration needed in an only-M system to
 129 obtain the same flux as in the system under study (where usually there are complexes
 130 which also contribute to the flux by dissociation).

131

132 Let us now consider a system with h ligands (denoted from 1L to hL) that can form h
 133 complexes. It can be shown -see eqn. (SI-21) in the Supporting Information of ^[30]- that,
 134 when M vanishes at $x=r$, the total flux can be formally written as

$$135 \quad J = \frac{D_M c_M^*}{g} + \sum_{j=1}^h \left[\frac{D_{M^jL} c_{M^jL}^*}{g} \left(1 - \frac{c_{M^jL}^r}{c_{M^jL}^*} \right) \right] = \frac{D_M c_M^* + \sum_j \xi_j D_{M^jL} c_{M^jL}^*}{g} \quad (10)$$

136 where

$$137 \quad \xi_j \equiv 1 - \frac{c_{M^jL}^r}{c_{M^jL}^*} \quad (11)$$

138 is labeled as the lability degree of the complex M^jL .^[31]

139

140 Comparison of eqn. (9) and (10) allows to solve for c_{DGT} :

$$141 \quad c_{DGT} = c_M^* + \sum_j \xi_j \frac{D_{M^jL}}{D_M} c_{M^jL}^* \quad (12)$$

142 which provides an interpretation of c_{DGT} in terms of the species present in the system:
 143 each species contributes to c_{DGT} with the equivalent free metal that gives the same
 144 contribution to the metal flux.

145

146 Notice that previous expressions hold even in the absence of ligand excess ($c_{M^jL}^* \gg c_M^*$
 147)^[29].

148

149 Now, if we assume that all diffusion coefficients are similar and that complexes can be
 150 just classified as either totally inert ($\xi=0$) or fully labile ($\xi=1$), one finds

$$151 \quad c_{DGT} \approx c_M^* + \sum_k^{fully\ labile} c_{M^kL}^* \quad (13)$$

152 which supports the basic notion that DGT is essentially measuring the labile fraction of
 153 the complexes^[2,32-34].

154 However, more rigorously, eqn. (12) indicates that c_{DGT} is the sum of labile
 155 concentrations *weighted* by the ratios of each complex diffusion coefficient with respect
 156 to D_M ^[22,33,35]. So one must resist the temptation of attributing all variations in c_{DGT} just
 157 to lability, while disregarding changes in mobility. As an example, consider a system with
 158 just one fully labile complex ($\xi=1$) with low mobility ($D_{ML}=0.01 D_M$) at a bulk

159 concentration overwhelming with respect to the free concentration $\left(\frac{D_{ML}}{D_M} c_{ML}^* \gg c_M^* \right)$.

160 According to eqn. (12), an experiment could yield $c_{DGT} = 0.01 c_{ML}^*$ even though the
 161 complex is labile. So, the retrieved c_{DGT} is not just the true labile concentration (which
 162 we know it is c_{ML}^*), but the labile concentration times the ratio of the complex over metal
 163 diffusion coefficient. One could even find cases where the diffusion coefficient of the
 164 formed complex is higher than the one of just metal (i.e. such as iodide with cadmium
 165 ^[36]) and obtain a DGT-concentration higher than the total one (i.e. $c_{DGT} > c_{ML}^* \approx c_{T,M}^*$).

166 Table 1 considers 4 cases with the same total metal, free metal and DGT concentrations
 167 for a mixture of two complexes. In the first 3 combinations, the concentration of both
 168 complexes is the same. In the first case, the contribution of both complexes to c_{DGT} is the

169 same, although complex 1 is only half-labile and mobile, while complex 2 is fully labile
170 but just half-mobile. In the second case, only complex 1 contributes, because M^2L is
171 immobile. In the third case, only complex 2 contributes, because M^1L is totally inert. In
172 case 4, we have $c_{M^2L}^* > c_{M^1L}^*$, but the contribution of the “super-mobile” complex 1 is
173 higher than the one of the quite immobile complex 2, whose labile fraction (5.74 nM) is
174 also higher than c_{DGT} (5.02 nM).

175

176 The use of c_{DGT} as the output of the DGT experiment has simplified the practical
177 manipulation of the result, while the high correlation between this measurement and
178 toxicity or availability experiments^[37] has boosted the popularity of DGT. This
179 correlation also indicates that fluxes play a key role in uptake or toxicity phenomena.^[38]

180

181 **4. Penetration of the complex into the resin layer**

182 The prediction of the flux in a system with just one complex taking into account the
183 kinetics of association/dissociation was initially based on assuming that the resin acted as
184 a “perfect sink” for the metal (i.e. $c_M=0$ for $x<=r$) and “perfect wall” for the complex (i.e.
185 null flux of ML at $x=r$). The so-called “voltammetric expressions”^[39] failed to reproduce
186 the experimental results^[40].

187 More refined numerical models^[22,24,41] introduced a new phenomenon: both M and ML
188 can diffuse in the resin layer (still considered ideally as a 1D domain with binding sites
189 evenly distributed). Due to “penetration”, the reaction layer, i. e., the layer where there is
190 net dissociation of the complex, extends from the gel domain into the resin domain, this
191 having a high impact on metal accumulation. These numerical models successfully fitted
192 the experimental results. They also led to the derivation of a simplified analytical
193 model^[41] with the help of additional hypotheses such as: i) perfect sink for M throughout

194 the resin layer (backed with experimental observations in ^[42,43]), and ii) excess of ligand
 195 L (i.e. the bulk concentration of M is much less than that of ML). The expressions of the
 196 analytical model reproduced the experimental results as the numerical simulations
 197 whenever the additional hypotheses held. Characteristic indicators of the penetration
 198 analytical model (PAM) are the penetration parameter λ_{ML} and the disequilibrium layer
 199 thickness m .

$$200 \quad \lambda_{ML} = \sqrt{\frac{D_{ML}}{k_d}} \quad (14)$$

201 is related to the distance of penetration of ML inside the resin. It can be seen as the
 202 intercept of the tangent of c_{ML} -profile at $x=r$ with the abscissae axis (i.e. zero ML
 203 concentration) and it is related to the thickness of the reaction layer in the resin domain.

$$204 \quad m = \sqrt{\frac{D_{ML}}{k_d(1 + \varepsilon K')}} \quad (15)$$

205 is a quantification of the thickness (within the gel phase) where c_M and c_{ML} are not in
 206 equilibrium in terms of the effective stability constant (i.e. the reaction layer in the gel
 207 domain),

$$208 \quad K' = Kc_L^* \quad (16)$$

209 and the normalized diffusion coefficient

$$210 \quad \varepsilon = \frac{D_{ML}}{D_M} \quad (17)$$

211 The flux can be expressed as

$$212 \quad J = \frac{D_M c_M^*}{g} + \frac{D_{ML} c_{ML}^*}{g} \xi = \frac{D_M c_M^*}{g} (1 + \varepsilon K' \xi) \quad (18)$$

213 with the lability degree being

$$\xi = 1 - \frac{c_{\text{ML}}^r}{c_{\text{ML}}^*} = 1 - \frac{(1 + \varepsilon K')}{\varepsilon K' + \frac{g}{m} \coth\left(\frac{g}{m}\right) + \frac{g}{\lambda_{\text{ML}}} (1 + \varepsilon K') \tanh\left(\frac{r}{\lambda_{\text{ML}}}\right)} \quad (19)$$

215

216 The availability of analytical expressions within PAM for the flux, the lability degree, the
 217 concentrations profiles, etc. allows gaining insights into the impact of the various
 218 physicochemical parameters. The plotting of the concentration profiles (such as those
 219 seen in Fig 1) allows one to visualize regions where equilibrium is practically fulfilled as
 220 the zones where the normalized concentrations collapse. In the shown case of CoNTA,
 221 the collapse almost reaches the interface resin/gel, reflecting a quite labile complex as
 222 also confirmed by the low value of c_{ML}^r (see eqn. (6)).

223 Previous studies, using PAM, have shown:

224 i) Neglecting penetration (e.g. using voltammetric expressions^[39]), seriously
 225 underestimates the lability of the complex^[40] or, in other words, the penetration into the
 226 resin *labilizes* the complex (i.e. DGT senses a much more labile fraction than
 227 voltammetric techniques).

228 ii) The change in the value g (around typical values) has a mild impact on J and on ξ
 229 ,^[41,44]

230 iii) The influence of the ligand concentration on the lability degree is mild (for ligand
 231 excess conditions).^[27,30]

232 iv) The variation of r can have a large effect^[40,41] and future experimental designs with
 233 resins of varying thickness are expected to further exploit this fact.

234

235 Experiments with 2 resin layers (also called double binding layers), denoted “back” and
 236 “front”, have already been used to probe the complex dissociation rates.^[43,45] Information
 237 gained from analytical expressions can be helpful not only as experimental guidelines,

238 but also for the numerical simulations (given the vast number of combination of
 239 parameters that might be necessary to explore to reach certain conclusions). For instance,
 240 with the PAM, and following a similar procedure to that used in ref. [42] for just metal,
 241 one can derive rigorous and approximate expressions for multilayer accumulations as
 242 shown next.

243 The number of moles accumulated in the front resin (extending from $x=r/2$ to $x=r$) can be
 244 computed as

$$245 \quad n_M^{\text{Front}} = tA \int_{r/2}^r k_d c_{\text{ML}}(x) dx + tAD_M \left. \frac{dc_M}{dx} \right|_{x=r} \quad (20)$$

246 and the moles in the back resin is

$$247 \quad n_M^{\text{Back}} = tA \int_0^{r/2} k_d c_{\text{ML}}(x) dx \quad (21)$$

248 where the entire flux of free metal arriving to the resin is assigned to the front layer. For
 249 the first right hand term of n_M^{Front} and for n_M^{Back} , integration is very easy because (see SI -
 250 9 in ref. [41])

$$251 \quad c_{\text{ML}}(x < r) = c_{\text{ML}}^r \frac{\cosh\left(\frac{x}{\lambda_{\text{ML}}}\right)}{\cosh\left(\frac{r}{\lambda_{\text{ML}}}\right)} \quad (22)$$

252 The flux of metal at the interphase (second term in the right hand side of (20)) can be
 253 computed combining SI-24 and SI-25 in ref. [41]. Thus, after simple algebra using c_{ML}^r
 254 given by eqn. SI-27 in ref. [41], only finally reaches

$$255 \quad \frac{n_M^{\text{Front}}}{n_M^{\text{Back}}} = 2 \cosh\left(\frac{r}{2\lambda_{\text{ML}}}\right) - 1 + \left[\frac{\lambda_{\text{ML}}}{m\varepsilon K'} \coth\left(\frac{g}{m}\right) + \frac{1}{\varepsilon K'} \tanh\frac{r}{\lambda_{\text{ML}}} \right] \frac{\cosh\left(\frac{r}{\lambda_{\text{ML}}}\right)}{\sinh\left(\frac{r}{2\lambda_{\text{ML}}}\right)} \quad (23)$$

256 It can be seen that the term in between the square brackets (corresponding to the
 257 contribution of metal dissociation in the gel) is negligible for typical parameter values.
 258 So,

$$259 \quad \frac{n_M^{\text{Front}}}{n_M^{\text{Back}}} = 2 \cosh\left(\frac{r}{2\lambda_{\text{ML}}}\right) - 1 \quad (24)$$

260 can be seen as a practical accurate simplified expression corresponding to just the
 261 dissociation of ML inside each of the two binding resins. Eqn (24) is not a good estimate
 262 of eqn. (23) for extremely inert complexes, as in this case the approximation cannot take
 263 into account that most of the arriving total metal goes to the front layer (because the
 264 dissociation in the resin layer becomes increasingly negligible). The discrepancies for
 265 some “pathological” cases can be seen in Fig. 2, where, in order to bound the variations
 266 in the range [0..1], the ratio of the front layer over the total amount of moles,

$$267 \quad \frac{n_M^{\text{Front}}}{n_M} = \frac{\frac{n_M^{\text{Front}}}{n_M^{\text{Back}}}}{\frac{n_M^{\text{Front}}}{n_M^{\text{Back}}} + 1} \text{ is represented for different } \lambda_{\text{ML}} \text{ values.}$$

268

269 For sufficiently large r -values (see cases of Co and Cd in Fig. 3), $\frac{n_M^{\text{Front}}}{n_M}$ tends to one, as

270 λ_{ML} will become much shorter than the thickness of the front resin layer. For intermediate

271 r -values, some ML will be able to reach the back resin layer and $\frac{n_M^{\text{Front}}}{n_M}$ can approach 0.5

272 (especially for very inert complexes). For very small r -values, the contribution of ML

273 dissociation in the resin phase will be negligible in front of the dissociation in the gel

274 domain (which is ascribed to bind to the front resin layer). Notice that it is for this small

275 r -values that the approximation (24) fails to consider that and it rather tends to $\frac{n_M^{\text{Front}}}{n_M} = 0.5$

276 For the CdNTA case (orange continuous line), a change in the resin thickness close to the
 277 typical value ($r=0.4$ mm) does not modify the ratio $\frac{n_M^{\text{Front}}}{n_M}$ from a value very close to 1,
 278 indicating that almost all metal gets bound at the front resin in agreement to the labile
 279 behavior of the CdNTA complex. So, this change cannot be used to find λ_{ML} and the
 280 kinetic information on CdNTA. Likewise, for a too inert case, $\frac{n_M^{\text{Front}}}{n_M} \approx 0.5$ and no reliable
 281 information other than $\lambda_{\text{ML}} \gg r$ can be obtained.

282 The region of transition from 0.5 to 1 can be quantified via a “characteristic resin
 283 thickness” from the ratio attaining the intermediate value 0.75. From $\frac{n_M^{\text{Front}}}{n_M} = 0.75$, using

284 eqn. (24) one finds that this characteristic resin thickness can be around

$$285 \quad 2 \operatorname{arccosh} 2 \lambda_{\text{ML}} \approx 2.63 \lambda_{\text{ML}} \quad (25)$$

286 Only the use of double resins whose total thickness is of the order of magnitude of $2 \lambda_{\text{ML}}$
 287 can yield values sufficiently different from 0.5 and 1 as to be used for retrieving kinetic
 288 information (taking into account typical experimental errors). In the cases used in Fig3,
 289 the λ_{ML} -values are 9.57×10^{-6} m for CdNTA, 2.19×10^{-4} m for CoNTA and 7.14×10^{-2} m
 290 for NiNTA. The kinetic parameters of too labile complexes (such as CdNTA) or too inert
 291 complexes (such as NiNTA) could not be accurately resolved with ordinary resins
 292 ($r=4 \times 10^{-4}$ m).

293 So, for a given resin thickness, there is a kinetic window of available information for the
 294 analysis based on (23) or (24). Conversely, up to certain extent, the thickness of the resin
 295 could be tuned^[46] to the characteristic resin length of the complex.

296 Apart from a preliminary exploration^[43], the potential practical use of (24) to retrieve the
297 kinetic parameter λ_{ML} has yet to be confirmed with further experiments in systems
298 fulfilling the hypotheses of PAM and overcoming technical difficulties.

299

300 **5. Mixtures**

301 Environmental samples are practically always a mixture of many components, of both
302 metal ions and ligands, giving rise to a distributed variety of equilibrium constants
303 (heterogeneity)^[44] and diffusion coefficients (polydispersity).

304

305 In principle, a *mixture of metal cations* (in combination with a homogeneous ligand) can
306 be dealt with in DGT as if each metal was alone, provided the excess of ligand conditions
307 apply for each one of the elements (i.e. negligible competition effects in the bulk). In this
308 way, the expressions in this work appearing up to here apply to each metal under the
309 corresponding assumptions.

310 As commented above, expression (10) holds for a *mixture of ligands* that react with a
311 metal in a set of parallel reactions regardless the ligand to metal ratio. The question now
312 is how the mixture impacts on the expression for the particular lability degree of each
313 complex arising in eqn. (10), i.e., can eqn. (19) be used in eqn. (10)? This question is of
314 high interest, since it would allow studying complex mixtures with information obtained
315 from single ligand systems.

316 In a mixture of ligands, the diffusion-reaction process of the species related to one ligand,
317 say 1L , is coupled to the diffusion-reaction processes of the species related to all other
318 ligands, because all the reaction systems are coupled through M ^[31,47,48]. So, a rigorous
319 approach requires numerical simulation. However, under ligand excess conditions with
320 the hypothesis of the resin being a perfect sink for the metal, then c_M becomes zero in the
321 resin phase and the coupling can only affect the gel phase. Within a wide range of

322 explored conditions, digital computations have indicated that the dissociation of
 323 complexes mostly occurs in the resin,^[30] so that the coupling in the gel domain is very
 324 mild. Thus, the rigorous expression (10) for the flux can be approximated, under ligand
 325 excess conditions, by replacing each individual lability degree ξ_j in the whole mixture
 326 (only accessible via intensive computation) with the lability degree ($\xi_j^{h=1}$) in an equivalent
 327 system where there was only the ligand jL (both ligand and metal at the same total
 328 concentrations as the original system).

$$329 \quad J^{h=1} = \frac{D_M c_M^* + \sum_j \xi_j^{h=1} D_{M'L} c_{M'L}^*}{g} \quad (26)$$

330 Thus $\xi_j^{h=1}$ can be computed with eqns. such as (19) (if there is no specific DBL to
 331 consider) or other more involved equations (if the solution has a very different behavior
 332 than the gel phase). This approximation has been shown more accurate than 10% for
 333 mixtures with devices having a g thicker than 0.8 mm^[30].

334

335 **6. Diffusive boundary layer: experiments varying the** 336 **thickness of the gel layer**

337 In fact, since DGT's presentation,^[1,32] it was recognized that convective movements in
 338 the solution would extend the diffusion domain with a “diffusive boundary layer”, DBL.
 339 Rigorously speaking, one should take into account the velocity profiles (for the various
 340 hydrodynamic regimes which might vary for different zones of solution in the proximity
 341 of the filter and for different experiments) and solve the pertaining continuity equation
 342 taking into account the flow term (see eqns. (21)-(34) in ^[49] and refs. ^[50,51]). Up to now,
 343 all treatments of DBL with DGT rely on Nernst diffusion layer concept: they assume that
 344 the real system is equivalent (regarding the final flux) to a virtual one where there is full
 345 stirring for $x > r + g + \delta$ (i.e. bulk conditions) and quiescent conditions in between $x = r + g$ and

346 $x=r+g+\delta$. This assumption might be especially critical because the “equivalence” for just
 347 M can be very different to the required equivalence for another system having also a given
 348 M^1L or a third system with a mixture of complexes (e.g. this equivalence might be
 349 dependent on the diffusion coefficients of the species presents in the mixture).^[49] Future
 350 work to establish the impact of the Nernst diffusion layer approximation is timely.
 351 All equations presented up to here remain valid in the case of any existing DBL provided
 352 that: i) Nernst diffusion layer concept is acceptable, ii) the diffusion coefficients of all
 353 species are acceptably similar in the gel and in the solution and iii) there are no Donnan
 354 partitioning effects between gel and solution (see section 7); in this case one should use
 355 an effective g resulting from the aggregated thicknesses of the gel, filter and DBL
 356 thicknesses.
 357 Experiments with varying gel thickness have been performed to estimate the physical
 358 length of the DBL^[32,52,53]. Several works^[12,25,50,51,54,55] tackled the determination of δ
 359 when $D_M \neq D_M^w$ and/or $D_{ML} \neq D_{ML}^w$ (superscript “w” indicates that the diffusion
 360 coefficient correspond to the solution -water phase; no superscript is used here for
 361 parameters in the diffusive gel although in the SI of ref^[25] the superscript “gel” was used).
 362 Imposing continuity of the fluxes and concentrations at the boundary gel-solution, and
 363 assuming equilibrium between M and ML in the solution, one arrives (see SI of^[25]) to:

$$364 \quad J = \frac{c_M^*}{\frac{\delta}{D_M^w(1+\varepsilon^w K')} + \frac{g + g_{\text{kin}}^p}{D_M(1+\varepsilon K')}} \quad (27)$$

365 where

$$366 \quad g_{\text{kin}}^p \equiv \frac{\varepsilon K' m \tanh \frac{g}{m}}{1 + \varepsilon K' m \left(\tanh \frac{g}{m} \right) \left(\frac{1}{\varepsilon K'} + 1 \right) \frac{1}{\lambda_{ML}} \tanh \frac{r}{\lambda_{ML}}} \quad (28)$$

367 can be seen as the equivalent extra length that would be necessary to add to the gel layer
 368 thickness to account for the decrease of accumulated metal due to the kinetic
 369 limitations.^[25]

370 Fig 4 shows that, for the chosen typical parameters, the impact of varying δ on the flux is
 371 rather mild, in agreement with experimental reports^[51]. As expected, the flux decreases
 372 when δ increases or the diffusion coefficients inside the gel decrease.

373 As seen in Fig 5, lability increases when the DBL thickness increases or the diffusion
 374 coefficient D_{ML} decreases in the gel: in both cases there is more “time” along which the
 375 complex can dissociate.

376 The representation of the inverse of the accumulated mass ^[25,32,33] in front of varying g
 377 can be used to experimentally estimate the thickness of the DBL and, more importantly,
 378 to find the dissociation rate constant in systems where the bold assumption of just one
 379 ligand is acceptable. In the case of penetrating complex, previous eqns. (27) and (28) (see
 380 also SI of ^[25]) can be recast as:

$$381 \quad \frac{1}{n_M} = \left[\frac{\delta}{D_M^w (1 + \varepsilon^w K') c_M^* A t} + \frac{g_{kin}^p}{D_M (1 + \varepsilon K') c_M^* A t} \right] + \frac{g}{D_M (1 + \varepsilon K') c_M^* A t} \quad (29)$$

382 Strictly speaking, g_{kin}^p is also dependent on g , as eqn. (28) indicates. In cases where this
 383 dependence was suspected to be strong, one could fit as free parameters δ , c_M^* and g_{kin}^p
 384 in eqn. (29) with at least 3 experimental points of accumulation (i.e. at least 3 pairs (n_M ,
 385 g)). Then, as g_{kin}^p can be written in terms of k_d (by using eqn. (14) and (15) to replace λ_{ML}
 386 and m), the value of k_d can be found.

387 However, for typical parameters, the dependence of g_{kin}^p on g is mild, whenever $g > 2m$,
 388 because the term $\tanh(g/m)$ tends to 1. For instance, for a rather inert complex such as
 389 NiNTA at a total concentration such as $K' = 60600$, $k_d = 7.710 \cdot 10^{-6} \text{ s}^{-1}$ (Eigen mechanism),

390 $D_M=7.07\times 10^{-10}$ and $D_{ML}=0.7\times D_M$, we compute $m=3.8\times 10^{-5}$ m which is much less than
 391 the usual g . (Notice however, that this m would be larger than the 0.01 mm extra-thin gel
 392 layer used in recent developments^[46] and whose rigorous treatment would require a
 393 modified version of the PAM because there is no equilibrium throughout the DBL, see
 394 assumption above equation (27)).

395 So, in systems with one homogeneous ligand and no further complications, one would
 396 expect the representation of $1/n_M$ to be linear with g , as prescribed by eqn. (29) with
 397 constant g_{kin}^p . The ratio of the intercept over the slope (obtained in the linear regression)
 398 is:

$$399 \quad \frac{i}{s} = \frac{D_M(1 + \varepsilon K')}{D_M^w(1 + \varepsilon^w K')} \delta + g_{kin}^p \quad (30)$$

400 which allows to find k_d from g_{kin}^p using eqn. (14) and (15) as described above. The
 401 representation of the so-called Apparent Diffusive Boundary Layers (i.e. $ADBL = \frac{D_M^w i}{D_M s}$
 402) for several metals is designated as “kinetic signature” of the mixture.^[33]

403

404 Fig 6 shows the good linearity that could be obtained in a case of Cd with NTA and Co
 405 with NTA. The parallelism between the practically straight lines is due to the similarity
 406 of the diffusion coefficients and the K' -values. The linear regression of 3 points (at single,
 407 double and triple the standard value of g) of the Co series yielded a ratio $i/s = 3.06\times 10^{-4}$
 408 m which, applying eqn. (30), yielded $g_{kin}^p = 2.26\times 10^{-4}$ m in full agreement with the directly
 409 computed value of g_{kin}^p .

410

411 Notice that, in the particular case where the diffusion coefficients in the gel and in the
412 solution are the same, the ratio i/s is just $\delta + g_{\text{kin}}^{\text{p}}$, and all the treatment applies without
413 any additional problem.

414

415 If the plot $1/n_{\text{M}}$ vs g clearly deviates from linearity, and kinetic reasons (i.e. a large
416 variation of $g_{\text{kin}}^{\text{p}}$ with g) can be discarded, it might be that: i) the assumption of having
417 just one ligand with one stability constant is a too crude one for the current system and
418 we have to deal with mixtures; ii) electrostatic effects might be distorting the equations
419 (see section 7, below); iii) ligand excess conditions might not apply; iv) the mild variation
420 of the accumulation with the gel thickness (not far from the analytical error) might
421 preclude any safe treatment of data (especially if sufficient replicates in the same
422 conditions are not available), etc.

423

424 It can be shown that, in systems with a finite DBL, eqn. (6) is an excellent approximation
425 for the usual parameters, provided there is an overwhelming contribution of the complex
426 to the total flux in comparison with that of the free metal (i.e. $\varepsilon K' \gg 1$).

427 **7. Electrostatic effects**

428 Given that the resin and gel phases include fixed charges in their polymeric structures,
429 electrostatic effects might arise.^[56] Potential differences between the resin/gel phases
430 and/or between the gel/solution phases or around the resin beads can develop (i.e.
431 electrostatic potential profiles). When Chelex is used as binding agent, electrostatic
432 effects of the resin are expected to be dominant in comparison to those due to the gel,
433 since the binding sites in the Chelex are charged. Local electrostatic potentials might
434 imply migration terms in the transport equations of charged species. Electrostatic effects
435 will be especially important at low ionic strengths, since otherwise these effects are

436 screened by the salt background. Rigorous solution requires, then, the application of the
 437 Nernst-Planck transport equations plus the Poisson equation. This is a cumbersome task,
 438 especially for a large number of charged species. A simple situation arises when the
 439 electrostatic potential can be considered constant within the solution and resin phases^[49]
 440 with potential jumps being restricted just at the interfaces (the Donnan potential). This
 441 can be a good approximation when the distance between charges is shorter than the Debye
 442 length and the influence of the charge of binding species on the Donnan potential is
 443 negligible. The Donnan potential difference increases with decreasing ionic strength of
 444 the system^[2,34] as indicated by the following expression valid for a symmetrical univalent
 445 background electrolyte yielding an ionic strength I :

$$446 \quad \Psi_{\text{resin}} - \Psi_{\text{solution}} = \frac{RT}{F} \operatorname{arcsinh} \left(\frac{\rho_{\text{charge, resin}}}{2I} \right) \quad (31)$$

447 where $\rho_{\text{charge, resin}}$ is the charge density in the resin (with its sign). A similar equation can
 448 be written between gel and solution when there is a net charge density in the gel.
 449 Donnan potential differences lead to Donnan partitioning effects, increasing the
 450 concentration of those ions with the opposite charge to that of the phase and decreasing
 451 those of the same charge. For instance, at 25°C, if the gel has a Donnan potential 5 mV
 452 more negative than the solution, then a divalent cation at the gel/solution interphase would
 453 have an equilibrium concentration at the gel side (designated as $x=(r+g)^+$) 1.48 times
 454 larger than at the solution side (designated as $x=(r+g)^-$) according to the equation:

$$455 \quad \Pi_{r+g, M} = \frac{c_M^{(r+g)^+}}{c_M^{(r+g)^-}} = \exp \left(\frac{z_M F (\Psi_{\text{gel}} - \Psi_{\text{solution}})}{RT} \right) \quad (32)$$

456 For solutions with just metals, the effect of the charges in the resin is expected to be
 457 negligible, since the metal concentration drops to negligible values at the resin-gel
 458 interface. However, relevant effects will arise for background cations, anions or charged

459 partially labile complexes. In the latter case, decreasing accumulations or increasing
460 accumulations when ionic strength decreases are expected ^[43].

461

462 Apart from implying preconcentration or exclusion of the determinand, electrostatic
463 effects might impact on the other species coupled to the analyte. For instance, humic acid
464 enrichment in the gel due to Donnan partitioning could be relevant for metal speciation. ^[34]

465

466 Donnan partitioning between a typical DGT gel layer and the solution seems to be of
467 limited impact for ionic strength higher than 1 mM, ^[2] but relevant for doped hydrogels. ^[57]

468

469 Electrostatic effects seem to be at the root of difficulties in systems with very low ionic
470 strength, such as Canadian lakes. ^[54] A full consideration of these phenomena, and the
471 consequences for the interpretation of DGT measurements, can be seen in ^[43]

472

473 **8. Limitations and challenges**

474

475 The list of issues ^[2] that can impact on the interpretations and models is large (and cannot
476 be exhaustive): lack of reproducibility in the DBL (changes in δ along the deployment
477 time of one experiment, and from one device to another device); change in the pressure
478 of the layers modifying the diffusion coefficients and their thicknesses; biofouling, ^[58]
479 different mixtures of ligands and metals changing along the deployment time or from
480 sampling site to sampling site; uncertainty of most parameters (such as diffusion
481 coefficients, tortuosity, ^[59] DBL thickness..); size discrimination of some complexes or
482 nanoparticles; ^[60,61] interactions between gels and analytes or ligands; ^[34,62] lack of

483 uniformity in the distribution of the beads in the resin layer; specificities of the filter;
484 improved geometry including edge effects;^[20,63] etc.

485

486 Independent determination of key parameters (e.g. resin capacity and thermodynamic
487 constants,^[64,65] etc.) can avoid overparametrization of the models of DGT just based on
488 its own data. Of special relevance is the issue of values of the dissociation rate constants.
489 Usually, Eigen mechanism^[66] has been assumed for the complex association rate, so that
490 k_d could be computed from the knowledge of the stability constant. However, especially
491 inside the resin, other kinetic mechanisms (different from the dissociative one) could also
492 be in operation^[43].

493

494 There could be an exploitation of the different time-regimes ^[27] including the initial
495 transient and the final equilibrium stage ^[16,26].

496

497 Despite the aim of a strong resin with infinity capacity, issues around saturation,
498 competitions by protons (pH effects)^[26,32,67] or by different metals^[68] need to be fully
499 addressed.

500

501 A complete consideration of the effects and the information obtained with varying some
502 parameter (e.g. the gel thickness,^[25,33] the resin thickness,^[42,45,46] total metal ^[44]) could
503 also shed important light on the studied systems.

504

505 The specific characteristics of other sorbent mechanisms (anions, As, etc.) and other
506 interacting phases (such as soils^[69,70] or plants^[71]) need to be considered and, thus,
507 corresponding models developed or improved.

508

509 It is clear, then, that fun in working with the multiple avenues opened by DGT is not
510 going to finish soon.

511 **9. Conclusions**

512 Physicochemical models are essential to interpret DGT results. For instance, eqn. (12)
513 indicates that c_{DGT} is the labile fraction weighted by diffusion coefficients and eqn. (8) is
514 a recipe for computing a lability degree (when the contribution of free metal is negligible)
515 as a normalized flux. Key phenomena identified up to date include: diffusion (in the resin,
516 the gel and the DBL), kinetics of complex association/dissociation, mixture and
517 electrostatic effects. A rigorous, complete, treatment of all these phenomena in an
518 integrated model can only be reached with numerical simulations. However, reasonable
519 assumptions (such as ligand excess, perfect sink for the metal in the resin, one-ligand
520 labilities as surrogate of individual labilities, Donnan partitioning, etc.) allow to reach the
521 model PAM with analytical solutions that: i) lead to a deeper understanding of the impact
522 of the parameters; and ii) facilitate the suggestions of new experimental strategies to
523 derive more robust information from DGT sensors. A crucial point, demanding sound
524 work, is the limitation of the considered phenomena to those strictly required (for a given
525 system), in order to simplify the expressions and be able to access to relevant information
526 without too many unknown parameters.

527 Apart from dealing rigorously with all cases, numerical simulation also allows for
528 checking the limits of validity of the application of the analytical models. But, both
529 theoretical approaches, analytical and numerical, can only progress if they are also in
530 close contact with experimental realities (including both synthetic solutions and natural
531 samples).

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759 **12. Tables**

760

761 Table 1 Hypothetical systems consisting of a metal M and two ligand ¹L and ²L sharing the same
 762 total metal concentration (10.02 nM), the same free metal concentration (0.02 nM) and resulting in
 763 a common expected *c*_{DGT} (5.02 nM), despite the very different nature of the relevant
 764 physicochemical processes.
 765

ξ_1	ε_1	$c_{M^1L}^*$ / nM	ξ_2	ε_2	$c_{M^2L}^*$ / nM	contrib 1 ^{a)} / nM	contrib 2 ^{a)} / nM	<i>c</i> _{DGT} / nM
0.5	1	5	1	0.50	5	2.5	2.5	5.02
1	1	5	1	0	5	5	0	5.02
0	1	5	1	1	5	0	5	5.02
1	1.4	3	0.82	0.14	7	4.2	0.80	5.02

766

767 Foot to table : $\varepsilon_j \equiv \frac{D_{M^jL}}{D_M}$. a) Contrib. 1 or 2: Contribution of complex *M*^{*j*}*L* to *c*_{DGT}, computed as

$$768 \xi_j \frac{D_{M^jL}}{D_M} c_{M^jL}^*$$

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773 Table 2 Numerical values of parameters in the figures.

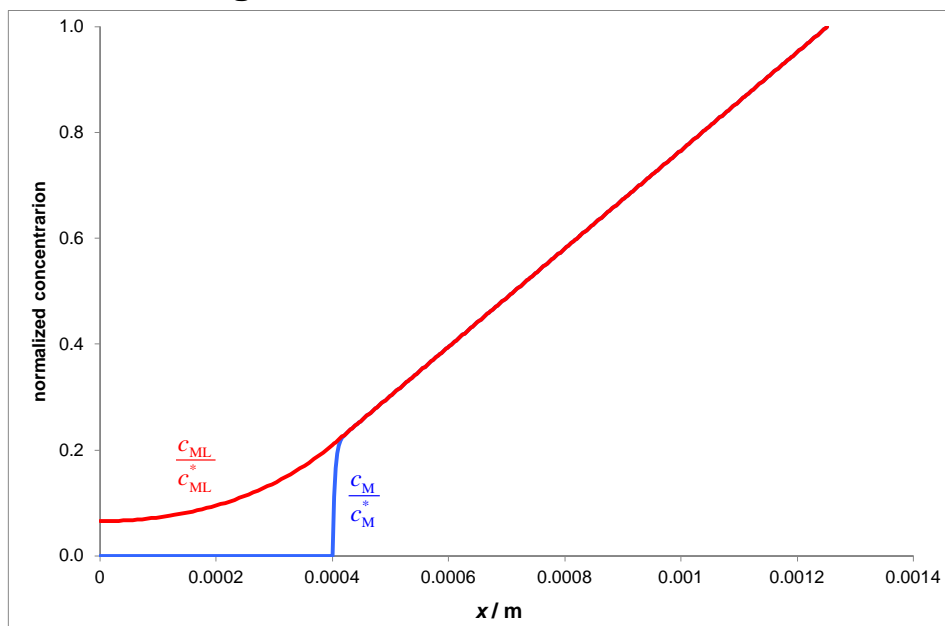
parameter	value
$c_{T,Cd}^*$	$10^{-2} \text{ mol m}^{-3}$
$c_{T,Co}^*$	$10^{-2} \text{ mol m}^{-3}$
$c_{T,Ni}^*$	$2.5 \times 10^{-2} \text{ mol m}^{-3}$
D_M (in gel)	$0.8 \times D_M^w$
D_{Cd}^w	$6.85 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
D_{Co}^w	$6.68 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
D_{Ni}^w	$7.07 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
D_{M-NTA} (in gel and resin)	εD_M
D_{M-NTA}^w	$\varepsilon^w D_{Co}^w$
g	$8.52 \times 10^{-3} \text{ m}$
$k_{d,Cd}$	4.19 s^{-1}
$k_{d,Co}$	0.00783 s^{-1}
$k_{d,Ni}$	$7.7 \times 10^{-6} \text{ s}^{-1}$
K' for Cd	1080
K' for Co	4490
K' for Ni	60600
r	$4 \times 10^{-4} \text{ m}$
δ	$1 \times 10^{-4} \text{ m}$
$\varepsilon = \varepsilon^w$	0.7

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13. Figures

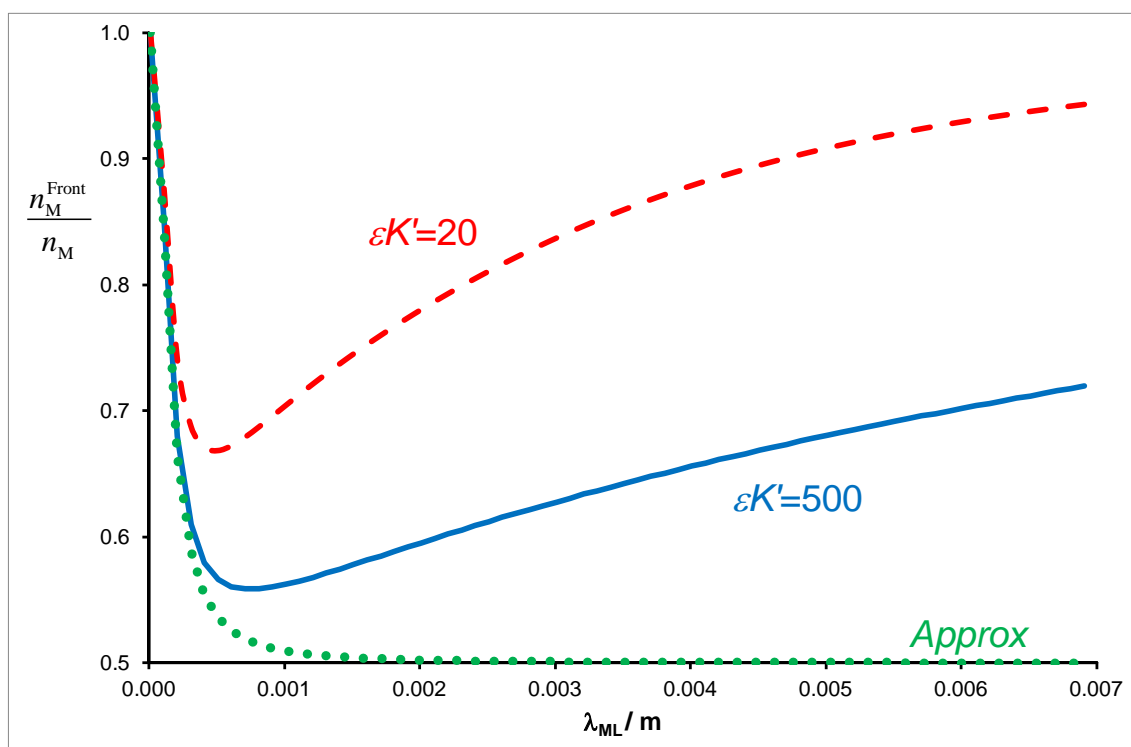


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778 Fig 1: Normalized concentration profiles of CoNTA with parameters in Table 2.

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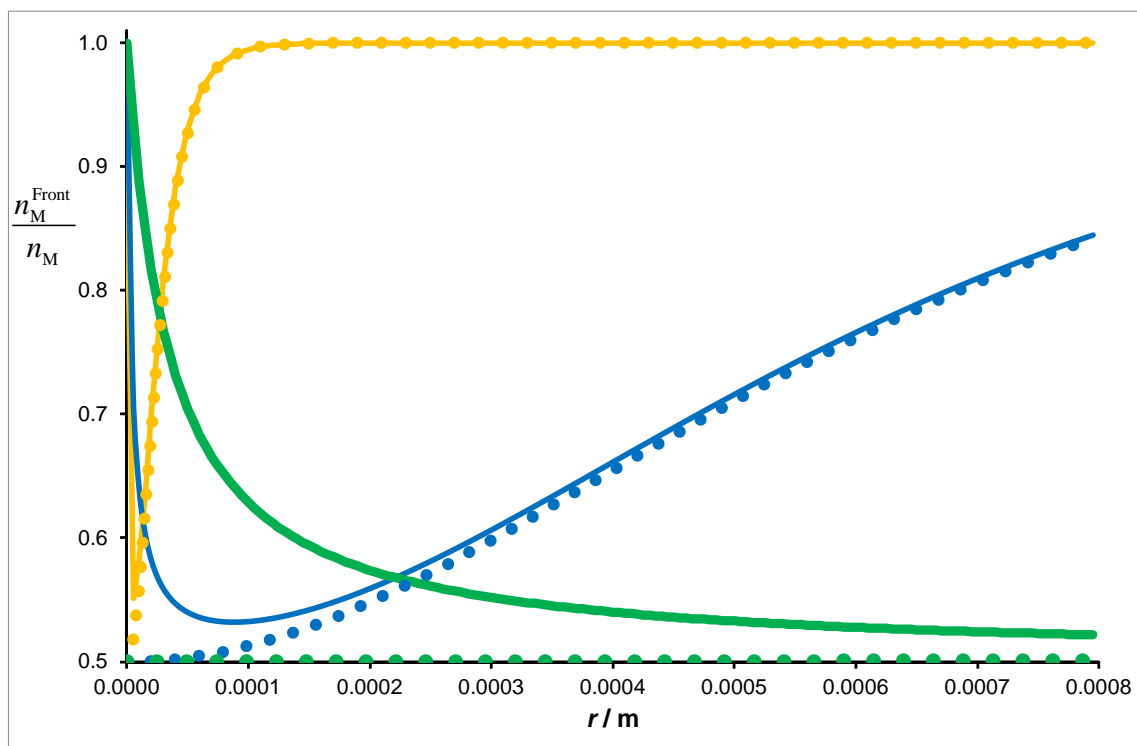


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783 *Fig 2: Ratio of accumulated number of moles of a metal M for different complexes with varying lability*
 784 *(from high lability at the left to low lability at the right) between the front layer (of thickness $r/2$) and*
 785 *the total number of moles accumulated by both binding layers. Rigorous expression (23) is used for*
 786 *$\epsilon K'=500$ in blue continuous line and for $\epsilon K'=20$ in red dashed line. Approximate expression (24) is*
 787 *plotted in green dotted line. Other parameters: $g=8.52 \times 10^{-4}$ m; $r=4 \times 10^{-4}$ m.*

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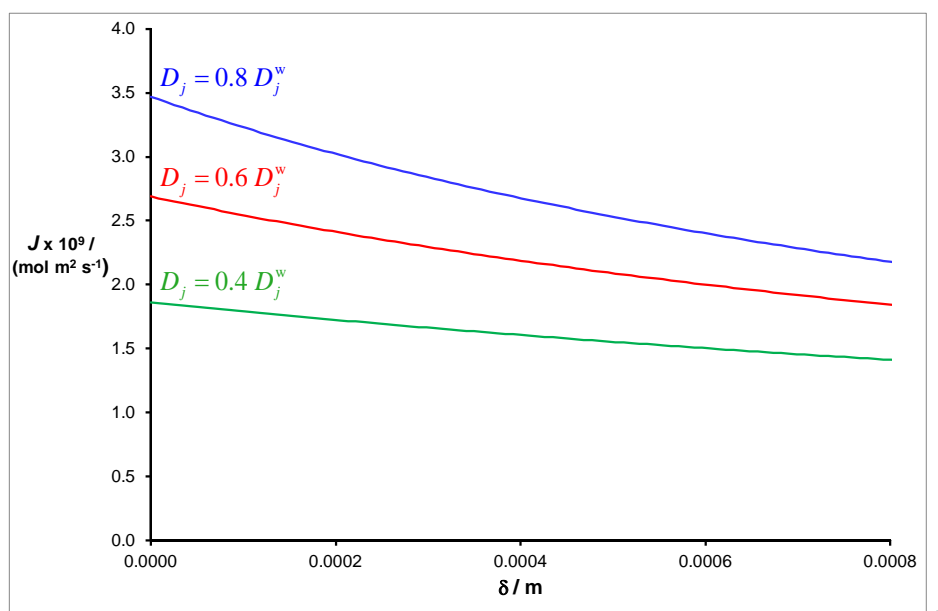


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794 *Fig 3: Ratio of moles of Cd (orange continuous line), Co (blue continuous line) or Ni (green continuous*
 795 *line) accumulated in the front layer with respect to the total number of moles accumulated in both*
 796 *layers vs. the total thickness of the resin ensemble computed with the rigorous expression (23). Values*
 797 *computed with the approximate expression (24) are represented as dotted lines in the same colour*
 798 *(for the case of Ni it is almost on top of the abscissae axis). Other parameters as in Table 2.*
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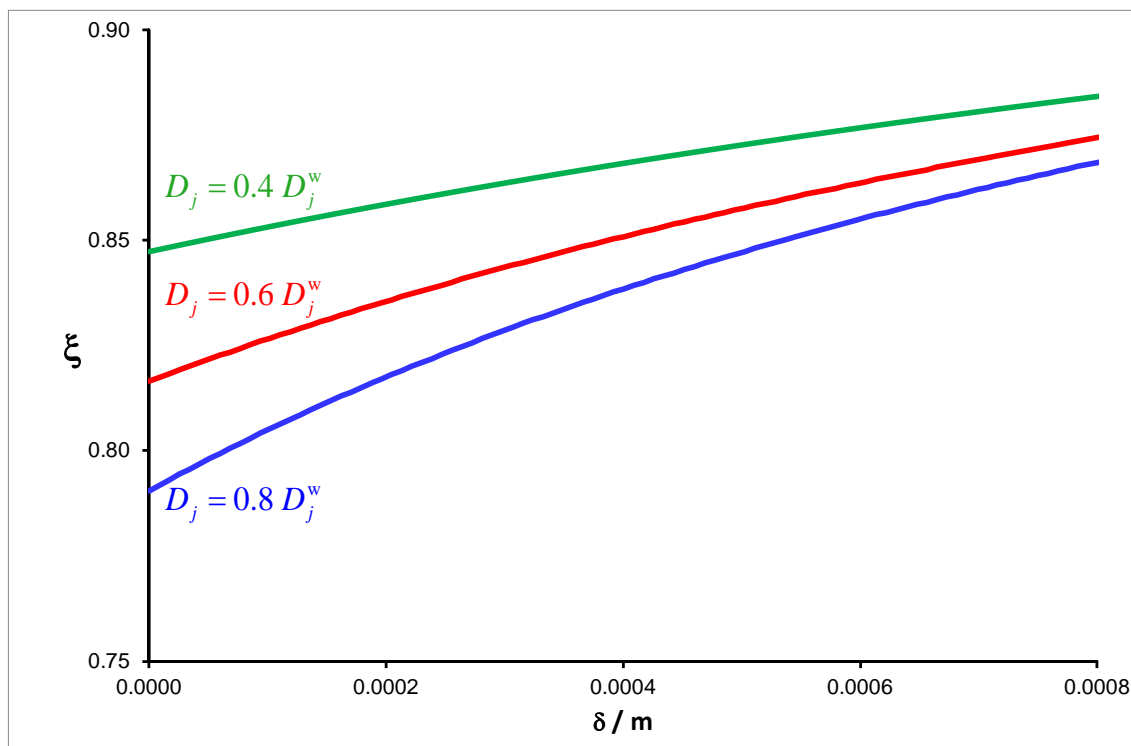


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802 *Fig 4: Impact of varying DBL thickness (δ) on the total flux of Co obtained in a system with one*
 803 *complex (CoNTA) as computed with the Penetration Analytical Model without electrostatic effects. The*
 804 *3 lines stand for different reductions^[34] (80%, 60% and 40%) in the diffusion coefficients of all species*
 805 *when entering the gel (with respect to an aqueous solution). See other parameters in Table 2.*

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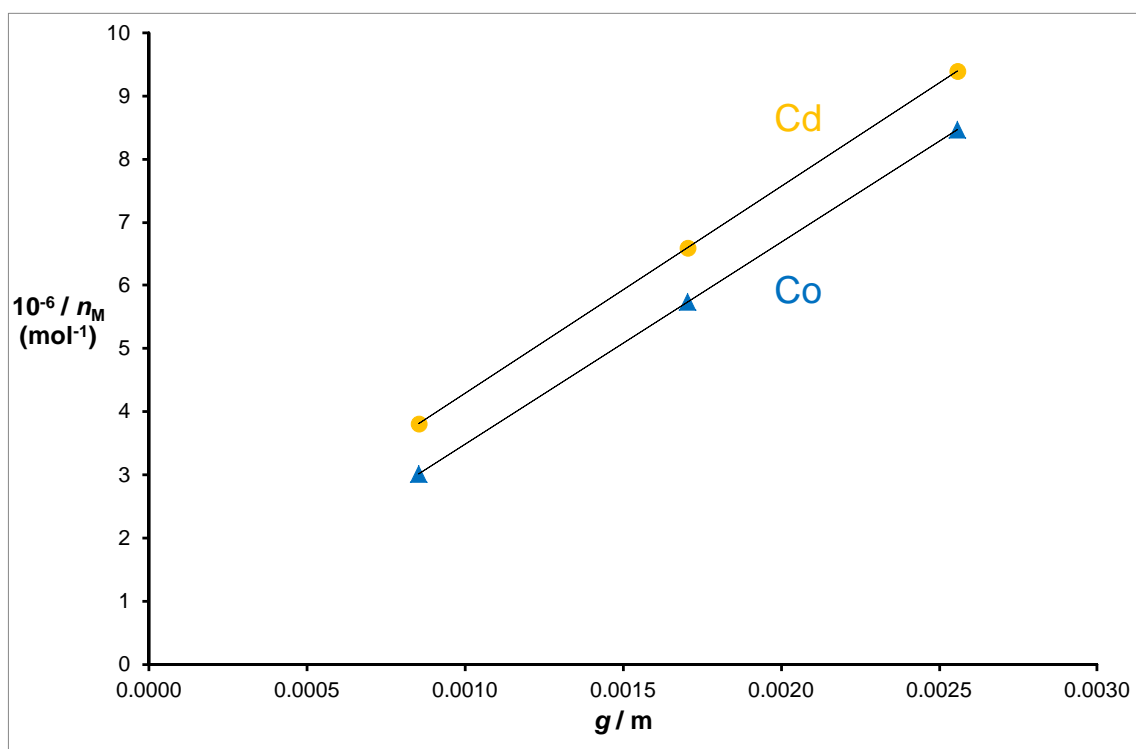


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808 *Fig 5: Impact of varying DBL thickness (δ) on the lability degree of CoNTA taking into account the*
809 *penetration into the resin. Conditions and parameters as in Fig 4.*

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813 *Fig 6: Plot of the inverse of the mass accumulated for increasing gel thicknesses in a system with*
 814 *CdNTA (orange circle markers) and CoNTA (blue triangle markers), showing a good linearity for these*
 815 *synthetic data (using one, two and three gels of thickness 8.52×10^{-4} m). This plot would allow the*
 816 *successful recovery of the kinetics parameters of CoNTA and CdNTA with eqn 30 if all other parameter*
 817 *values were known. Area= 3.14×10^{-4} m; time= 3 days. Other parameters as in table 2.*

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