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1 Minimization of the environmental impact of chrome tanning: a
2 new process reusing the tanning floats

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12

13

14 **Abstract**

15

16 A chrome tanning process which allows the reuse of tanning floats has been
17 developed. The most commonly used chromium salts were replaced by highly masked
18 and basified ones. This substitution eliminates basification operation and prevents pH
19 change and the considerable neutral salts concentration increase in the tanning float.
20 Consequently, tanning float can be reused several times. An optimum chromium salt
21 concentration in the tanning float between 10% and 12.5% has been determined. It has
22 been shown that the number of times the tanning float can be reused depends on the
23 quality of the leather grain to be manufactured. In the best case, a saving of 18L of

24 water per kilogram of tanned leather is calculated. This means savings of 90% of water
25 normally used.

26

27 *Keywords: Tanning industry, Chrome tanning, Tanning wastewater, Residual float,*
28 *Wastewater minimization.*

29

30 **1. Introduction**

31

32 Currently, minimizing the environmental impact of tanning processes is the goal
33 of many researchers (Gutterres et al., 2010; Li et al., 2010; Galiana et al., 2011; Jian et
34 al., 2011; Hu et al., 2011).

35 One of the environmental problems inherent in the chrome tanning is the
36 residual float generated. Specifically, 70% of total chrome (III) is discharged during this
37 process (IULTCS, 2008). This entails using large quantities of water that will end up
38 being transformed into highly contaminant wastewater (Simpson et al., 2001;
39 Saravanabhavan et al., 2003; Thanikaivelan et al., 2004). Data provided by various
40 prestigious international organizations (FAO, 2010; IULTCS, 2008) allow deducing that
41 approximately 17 million m³ of contaminated water is released yearly, with contents
42 0.04Mt Cr (III) approximately. This calculation is based on the pollution values from
43 tannery processes under good practice conditions. Therefore, it is reasonable to assume
44 that wastewater and chromium released in tanneries are much higher than the amounts
45 mentioned above. It is important to note that the consumption of water per kilogram of
46 tanned hide or skin can vary dramatically depending on the hide or skin type: from 2L
47 to obtain bovine leather for shoes to 20L for double-face fur.

48 Different solutions have been proposed in order to minimize this problem, but
49 without rejecting the use of chromium salts as a tanning material, because of the unique
50 properties that these salts confer on the leather. The reason is that these salts give the
51 leather unique properties. One of these solutions is recycling tanning floats (Cranston et
52 al., 1997; Aloy et Vuillermet, 1998; Tobin and Roux, 1998; Song et al., 2000; Scholz
53 and Lucas, 2003). However, this solution entails some drawbacks. If a standard process
54 is followed, tanning with the most commonly chromium salts used (33% basicity) to fix
55 the chromium in the collagen fibres of the hide, a pH increase, known as basification
56 within tanners, is necessary (Heidemann, 1993; Morera, 2000). This process is done
57 either by adding an alkali (solid or liquid) to the float or using self-basifying chromium
58 salts in which the alkali is already built in. In any case, the residual float cannot be
59 reused directly, because its characteristics (e.g. pH or higher amount of neutral salts in
60 the float) are not appropriate to begin the tanning process because the leather obtained
61 would present a poor appearance and would not meet the required physical properties.
62 One possible partial solution is to adjust the tanning float to the appropriate conditions
63 prior to tanning (e.g. lowering the pH with acid). This solution has several drawbacks.
64 Among them, it is a cumbersome process and the addition of alkalis and acids leads to
65 increase even more the amount of salts in the float. This result in a decrease of the
66 organoleptic properties of the leather grain's obtained.

67 A possible alternative to avoid the basification is the replacement of the most
68 commonly used chromium salts by highly masked and basified ones (66% basicity).
69 The interaction between an unmasked chromium salt of 33% basicity and the collagen
70 carboxylic groups is shown in Figure 1. To increase the chromium salt basicity means
71 replacing water groups in the chromium complex by hydroxyl groups. Then, larger
72 complexes with more atoms of chromium are made. Therefore, more chromium can be

73 fixed in the hide. Moreover, masking means the replacement of water groups in the
74 chromium complex by organic groups (e.g. acetate). This implies higher stability of the
75 chromium complex with respect to a pH increase, reducing the risk of precipitation of
76 chromium salt in the tanning float instead of their absorption in the hide. To work at
77 higher pH values means having more carboxylic groups (P-COO^{\ominus}) in the side chains of
78 collagen, the protein of the hide. Therefore, by increasing the number of points where
79 links between the hide and the chromium complexes can be established, more
80 chromium can be fixed in the hide.

81 Therefore, if chromium salts of high basicity are used to tan, it is not necessary
82 to increase the pH of the tanning float. This prevents the alkali addition each time a
83 batch of skins is tanned and its resulting increase in pollution load.

84 Consequently, these salts allow, under certain operating conditions, the direct
85 reuse of the tanning float, without cumbersome adjustments of pH. Another feature of
86 such salts is that tanning with temperatures at or above 50°C, the hide absorbs
87 significantly higher amounts of chromium than if the tannage is done at lower
88 temperatures. However, these chromium salts have also incorporated other salts (e.g.
89 sodium sulphate). The consequence is that the amount of salts in the tanning float will
90 increase each time the float is reused. This will increase the final amount of salts in the
91 leather and an important decrease in the organoleptic properties of the grain. However,
92 the increased concentration of salts in the float will be gradual and the same float can be
93 reused several times without affecting the quality of leather obtained. This is especially
94 true in those leathers in which the grain quality is relatively important, such as double-
95 face leathers, splits, pigment finished leather, etc.

96 The aim of this study is to develop a tanning system with a highly masked and
97 basified chromium salt and examine both the evolution of the tanning float, reusing it

98 several times, and the leathers obtained, in order to determine the advantages and the
99 limitations of such system.

100

101 **2. Materials and methods**

102

103 **2.1. Material**

104

105 The tanning process was carried out in a stainless steel tank with a stirring
106 paddle attached. The capacity of the tank is 8L and also incorporates an electrical
107 resistance and a thermostat to control the temperature of the tanning float. The tests
108 were carried out using pieces of split pickled bovine hide (pH = 3.5; 300mm X 300mm
109 X 3mm approx.). A commercial chromium salt (20% Cr₂O₃ and 66% basicity) was used
110 to tan. Laboratory grade chemicals were used for analysis.

111

112 **2.2. Methodology**

113

114 The research was carried out in two stages. In the first stage, the appropriate
115 concentration of the tanning float was determined. In the second stage, changes in the
116 tanning float and changes in the leathers obtained, related with the number of times the
117 tanning float had been reused, were investigated. For both stages the same tanning
118 procedure was followed.

119

120 *2.2.1. Tanning float preparation and tanning methodology*

121

122 To prepare the tanning float, the required amount of chromium salt was
123 dissolved in 5L of water. Once prepared, the solution was left to stand for one week in
124 order to stabilize it. Once prepared and pH controlled, the tanning float was introduced
125 in the stainless steel tank. The stirring paddle was started both to maintain the
126 homogeneity of the solution and to give it a slight mechanical effect. The electrical
127 resistance was started and the thermostat was graduated at 50°C. Finally, the piece of
128 hide was submerged and left in the tanning float for three hours. Then, the piece of hide
129 was taken out, washed slightly, let inside a plastic bag for a week and dried.

130

131 *2.2.2. Determination of the tanning float appropriate concentration*

132

133 Five tanning processes with different concentrations of chromium salt were
134 carried out. The chromium salt concentrations tested were 10%, 12.5%, 15%, 17.5%
135 and 20%. The percentage indicates the ratio weight of salt/water volume. The objective
136 was to determine the appropriate chromium concentration of the tanning float for
137 carrying out the tests of the second stage of experimentation.

138

139 *2.2.3. Reuse effect on the leather and on the tanning float*

140

141 Twenty successive tanning processes were carried out in the same float. The
142 chromium concentration in the initial float was chosen from the results of tests carried
143 out in the first stage of experimentation. The influence of certain physical, chemical and
144 organoleptic properties on the leathers obtained and on the evolution of the tanning float
145 was determined in order to assess the number of the tanning float possible reuses. The
146 relevant analysis was performed after 1, 5, 10, 15 and 20 tanning processes.

147

148 *2.2.4. Chemical analyses and physical test*

149

150 Float samples collected for analysis were filtered through a filter paper and the
151 corresponding analyses were performed. The chemical analyses and physical tests
152 carried out, with the methods followed, are detailed below:

- 153 • ISO 2419:2006. Sample preparation and conditioning (ISO, 2006).
- 154 • ISO 2418:2002. Sampling location (ISO, 2002).
- 155 • ISO 3380:2002 (modified). Determination of shrinkage temperature up to 100
156 degree C. Method was modified replacing water by glycerine (ISO, 2002a).
- 157 • ISO 5398:2007. Determination of chromium oxide content (ISO, 2007).
- 158 • ASTM D-5356-93. Standard test method for pH of chrome tanning solutions
159 (ASTM, 2009a).
- 160 • ASTM D-3898-93. Standard test method for chromic oxide in basic chromium
161 tanning liquors (ASTM, 2009).
- 162 • ISO 4684:2005. Determination of volatile matter. (ISO, 2005).
- 163 • ISO 4047:1977. Determination of sulphated total ash and sulphated water-
164 insoluble ash. (ISO, 1977).
- 165 • Float density. Directly measured with a densimeter.

166

167 **3. Results and Discussion**

168

169 **3.1. Determination of the tanning float appropriate concentration**

170

171 Results are shown in Table 1. Both the shrinkage temperature and chromium
172 content absorbed by the hide increase when the concentration of chromium salt
173 increases from 10% to 12.5%. In contrast, an increase of this concentration does not
174 cause changes in the properties analyzed. The adequate concentration of chromium salt
175 sought would be any value between 10% and 12.5% because, for most industrial goods,
176 a 4% Cr₂O₃ content in leather is enough. A concentration of 12% chromium salt was
177 chosen to perform the tests to assess the number of the tanning float possible reuses
178 (explained in section 2.2.3). This concentration ensures obtaining leathers with a high
179 tanning degree.

180

181 **3.2. Reuse effect on the leather and on the tanning float**

182

183 From the results obtained, some additional calculations were made to better
184 interpret the reuse effect. The organic matter in the tanning float was calculated using
185 formula (1):

$$186 \quad \text{Organic matter (\%)} = \text{Total Solids (\%)} - \text{Ashes (\%)} \quad (1)$$

187 Where: Total solids: Porcentaje del baño curtiente que queda en forma sólida
188 después de calentarlo a 103°C and Ashes: Parte del baño curtiente que queda en forma
189 sólida después de calentar los Total solids a 600°C.

190 Where: Total solids: Porcentaje of the tanning float which remains as solid after
191 heating at 103°C and Ashes: Part of the tanning float which remains as solid after
192 heating the Total solids at 600°C.

193

194 The inorganic matter (except the chromium oxide) in the tanning float was
195 calculated using formula (2):

196
$$\text{Inorganic matter (\%)} = \text{Ashes (\%)} - \text{Cr}_2\text{O}_3 \text{ in float (\%)} \quad (2)$$

197 Results are shown in Table 2.

198 Depending on the number of reuses of the tanning float, the results can be
199 explained as follows:

200

201 *3.2.1. Shrinkage temperature and chromium in leather*

202

203 The shrinkage temperature remained almost constant in all the leathers while its
204 chromium content increased as more reused was the tanning float. During the first five
205 float reuses, the hide absorbed approximately the same amount of chromium. By
206 increasing the number of reuses, the hide increased the absorption of chromium, but not
207 its fixation. Two facts support this conclusion. The first is the constant values of the
208 shrinkage temperatures. The second is that when the first five samples were immersed
209 in water to soak and subsequently measure the shrinkage temperature, no change in
210 colour of the water was observed while, from sample 11 to 20, the water was tinted
211 green, becoming darker. A likely explanation for this effect is that when the number of
212 float reuses increases, the float volume decreases, probably due to a simple effect of
213 evaporation. The increased absorption of chromium by the hide is due to the increased
214 concentration of chromium in the tanning float. However, its fixation is limited because
215 it depends on the chemically reactive groups the hide has.

216

217 *3.2.2. Evolution of the tanning floats composition*

218

219 Chemical analyses carried out allow distinguishing three parameters: chromium,
220 organic matter (coming from the masking compounds of the chromium salt) and

221 inorganic matter (coming from inorganic salts such sulphates incorporated into the
222 chromium salt). When increasing the number of reuses of the tanning float, the values
223 of the three parameters increase exponentially, following the same trend.

224 Very similar values of chromium oxide and organic matter were obtained. But
225 the exponential growth of inorganic values was much faster. This growth trend is
226 represented in Figure 2.

227 Therefore, as the tanning float is reused, chromium content, inorganic and
228 organic matters increase. This increase is also due to the decrease in the amount of
229 water in the float. However, proportionally, the absorption of chromium and masking
230 agents by the leather is superior to that of inorganic matter. Consequently, the inorganic
231 matter in the tanning float presents a greater exponentially increases.

232 It is also important to note that when the tanning float sample reused 20 times
233 was filtered, prior to its analysis, it began to crystallize almost immediately. Two types
234 of fully differentiated crystals were obtained: green and white ones. This phenomenon
235 was less pronounced in the float samples reused 15 and 10 times and almost zero in
236 both the float sample reused 5 times and in the float sample used in the first tanning.
237 The different types of crystals are explained according to the chromium salt used, that
238 contains 20% of chromium oxide and a large amount of other salts (e.g. sodium
239 sulphate) that precipitate as white crystals.

240 Another parameter that was monitored was the density of the floats. The results
241 were consistent with those cited in the preceding paragraphs. Indeed, the density also
242 increased exponentially when the numbers of reuses of the tanning float increased.

243 Finally, the pH variation of the tanning float was also logical; the tanning float
244 was acidified each time it was reused. By increasing the chromium compounds
245 concentration in the float, the pH was decreased.

246

247 *3.2.3. Organoleptic control of the leather pieces obtained*

248

249 The grains of the leather pieces obtained after tannage in floats reused up to five
250 times had a good fineness of grain. In the pieces obtained in subsequent tanning
251 processes a worsening of the grains was observed; they lost fineness and became rough.
252 After the tenth tannage, the leather pieces presented salt efflorescence. This
253 efflorescence increased as tanning float is reused. This loss of fineness of grain and the
254 subsequent salt efflorescence appearance are the result of progressive increase in the
255 concentration of inorganic matter (e.g. sulphates) in the tanning float. A higher
256 concentration of inorganic matter in the float implies more absorption of the pieces of
257 leather and thus more salt will precipitate and more salt efflorescence will appear.

258 Given these results, it is clear that what mainly limits of the tanning float reuse is
259 the amount of inorganic salts in the chromium salt. Depending on the type of leather
260 you want to make will vary the number of possible float reuses. The maximum savings
261 in water consumption (90%) will be achieved in the manufacture of leathers that require
262 a large consumption of water and those which the appearance of the grain is not
263 important. For example, extrapolating the results to the tanning of sheepskins for a
264 double-face fur, a saving of 18L of water per kilogram of tanned leather is calculated.
265 This figure was calculated taking into account that 20L of water per kilogram of skin
266 are commonly used in this type of tanning. Therefore, if the traditional way to tan is
267 followed, without recirculating the tanning float, and assuming that 1 kg of skin is
268 tanned in each tanning float, 200L of water are needed for tanning 10 kg of skins. If the
269 proposed new method is followed using the same tanning float for ten consecutive
270 tannages, only 20L of water is needed to tan 10 kg of skin because it will not be

271 necessary to change the tanning float. Therefore, to tan the same amount of skins, with
272 the new proposed method 90% less water than tanning with the traditional method is
273 used.

274 In this case, although the float is recirculated, the amount of chromium
275 discharged is the same as when using the traditional method. Chromium supply in the
276 traditional method is ten times smaller (Soler, 2002) than chromium supply in the new
277 method tested. By reusing the float 10 times, total chromium discharge per kilogram of
278 sheepskin is the same in both working systems. However, the proposed new tanning
279 method generates nine times less wastewater, thus dropping water treatment costs
280 significantly.

281 In addition to significant water savings, the proposed tanning method presents
282 another environmental benefit: by not adding alkalis to the tanning float the amount of
283 salts in wastewater substantially decreases and treatment in the sewage plants is easier.

284

285

286 **4. Conclusions**

287

288 With the chromium salt used and in test conditions, tannage can be done without
289 the basification operation. Leather can be easily obtained with chromium content and
290 shrinkage temperature exceeding usual commercial requirements. The tanning float can
291 be reused several times depending on the quality of the leather grain to be
292 manufactured. For all these reasons, the tested tanning method can be used to save
293 water, especially for the goods in which the appearance of the grain is not important, for
294 example in the cases of double-face furs, pigment finished leather or splits.

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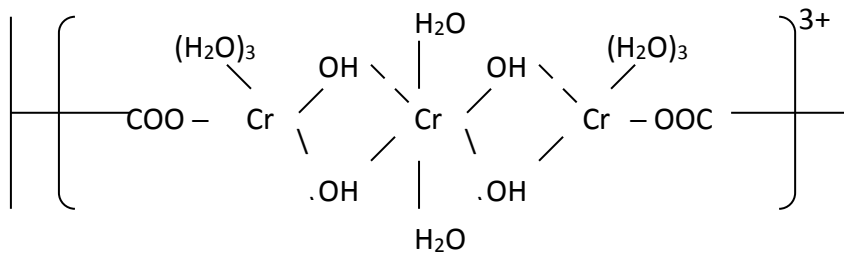
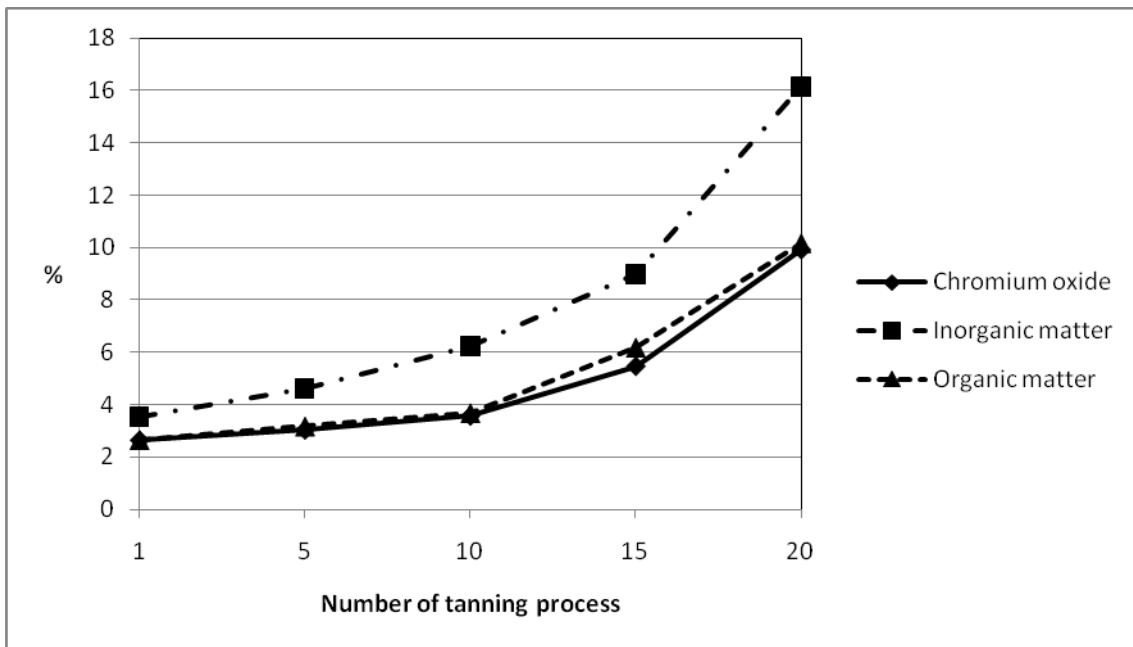


Fig. 1. Reaction between the chrome complexes and the collagen carboxylic groups



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384 Fig. 2. Evolution of the tanning floats composition

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Table 1

Results of physical tests and chemical analysis performed on the leather and on the tanning float

Chromium salt in tanning float (%)	Final pH of the tanning float	Shrinkage temperature (°C)	Cr ₂ O ₃ in leather (%)
10	3.42	118	2.6
12.5	3.42	128	4.4
15	3.42	131	4.2
17.5	3.42	127	4.3
20	3.41	126	5.3

393

394

395

Table 2

Results of physical tests and chemical analysis performed on the leather and on the tanning float

Number of tanning process	1	5	10	15	20
Shrinkage temperature (°C)	125	125	126	126	126
Cr ₂ O ₃ in leather (%)	4.8	4.9	5.4	5.6	7.3
Cr ₂ O ₃ in float (%)	2.7	3.1	3.6	5.5	9.9
Total dried solids (%)	8.9	10.9	13.5	20.6	36.2
Ashes (%)	6.2	7.7	9.8	14.4	26.0
Final float pH	3.60	3.62	3.57	3.51	3.31

Float density (g/mL)	1.06	1.08	1.10	1.16	1.33
Organic matter (%)	2.7	3.2	3.7	6.2	10.2
Inorganic matter (%)	3.6	4.6	6.2	9.0	16.1

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